

G.C.E. (Advanced Level) Examination - August 2001
PHYSICS - I
Provisional Scheme of Marking

2001 - Answers					
01	1	☒	3	4	5
02	1	2	☒	4	5
03	☒	2	3	4	5
04	1	2	3	☒	5
05	1	2	3	4	☒
06	1	2	3	☒	5
07	1	2	☒	4	5
08	☒	2	3	4	5
09	1	2	3	☒	5
10	1	2	3	4	☒
11	1	2	☒	4	5
12	1	2	☒	4	5
13	1	☒	3	4	5
14	1	2	3	☒	5
15	1	☒	3	4	5
16	☒	2	3	4	5
17	1	2	3	☒	5
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27	1	2	☒	4	5
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30	1	2	☒	4	5
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47	☒	2	3	4	5
48	1	2	3	4	☒
49	☒	2	3	4	5
50	1	2	3	4	☒
51	1	2	☒	4	5
52	1	☒	3	4	5
53	1	2	3	4	☒
54	☒	2	3	4	5
55	☒	2	3	4	5
56	1	2	☒	4	5
57	1	2	3	4	☒
58	1	2	3	☒	5
59	☒	2	3	4	5
60	☒	2	3	4	5

G.C.E. (Advanced Level) Examination - August 2001

PHYSICS - II

Provisional Scheme of Marking

A - PART

01. (a) 0.15 kg

(b) $F = \mu R$

(i)	R(N)	l(mm)	F(N)
block without any weight	1.5	25	1.0
block + 0.1 kg weight	2.5	30	1.5
block + 0.2 kg weight	3.5	35	2.0
block + 0.3 kg weight	4.5	41	2.6 ± 0.1
block + 0.4 kg weight	5.5	48	3.3 ± 0.1
block + 0.5 kg weight	6.5	55	4.0

For the correct list of R values

01

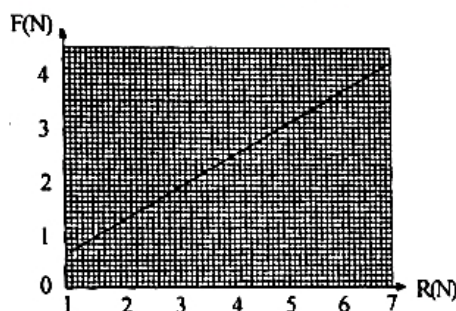
For the correct list of F values

02

(all correct - 02, any three correct 01)

(ii) Marking points correctly on the graph.

01



(iii) Drawing the best straight line

01

(iv) Gradient = $\frac{(3.3 - 1.5)}{(5.5 - 2.5)}$

$$\mu = 0.6$$

01

01

(d) Place a Convenient scale mark (e.g zero) of the ruler at the end of spring attached to the hook and take the reading of the other end.

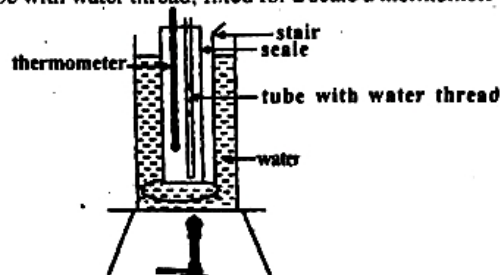
OR

Place the ruler by the side of the spring and take readings at both ends of it.

01

(02) (a) tube with water thread, fixed for a scale a thermometer

01



01

(b) Heat the tube dip the open end in water and allow it to cool down.

01

(c) middle of the tube

01

reasons - length of the air column is reasonably long and it will remain inside the water bath as well

OR

the water thread has to remain inside the tube

01

(d) Increase - the temperature of water slowly and measure the temperature of the water bath and the Corresponding length of the air column.

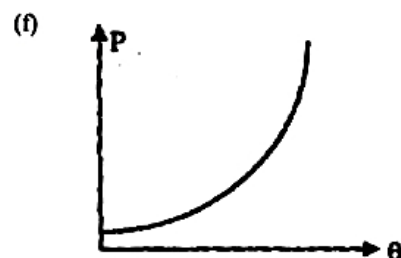
- 01

(e) (i) $P - P_1$ and $P - P_2$

$$(ii) \frac{(p - p_1) l_1}{\theta_1 + 273} = \frac{(p - p_2) l_2}{\theta_2 + 273}$$

02

(273 is not added of θ 01 mark)



01

03. (a) (i) Place the pin Q Close to the face AB

(ii) Place P and Q Pins sufficiently apart.

any one 01

(b) (i) look through the face AC and fix two pins to be in line with the images of P and Q.

01

(ii) The emergent ray Cannot be traced with one pin

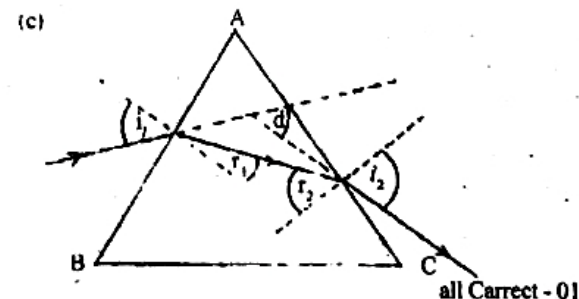
OR

to draw a straight line at least two points are required

OR

large number of lines Can be drawn through a Single point.

01



all Carrect - 01

$$(d) \quad d = (i_1 - r_1) + (i_2 - r_2) \quad R$$

$$d = (i_1 + i_2) - (r_1 + r_2)$$

01

$$(e) (i) \quad n = \frac{\sin 10^\circ}{\sin 6^\circ}$$

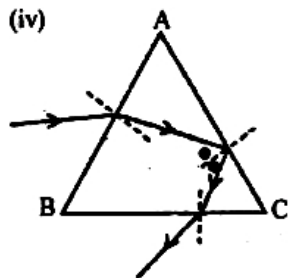
$$n = 1.6$$

01

$$\begin{aligned} \text{(ii)} \quad r_1 + r_2 &= A \\ r_2 &= 60^\circ - 6^\circ \\ r_1 &= 54^\circ \end{aligned}$$

(iii) No r_2 is greater than the critical angle of glass.
OR $r_2 > C$

(iv)



Total internal reflection - 01
Rest of the path - 01

(04) (a) From one side to the other OR
From left to right OR
From negative to positive OR
the deflection passes through zero

(b) (i) I_1 and I_2

(ii) Zero

(iii) $V_{AB} = V_{AD}$

$V_{BC} = V_{DC}$

(iv) $V_{AB} = I_1 R_1$ $V_{BC} = I_1 R_3$

$V_{AD} = I_2 R_2$ $V_{DC} = I_4 R_4$

(v) $I_1 R_1 = I_2 R_2$ and $I R_3 = I_4 R_4$

$$\frac{R_1}{R_3} = \frac{R_2}{R_4}$$

$$\Rightarrow R_4 = \frac{R_2}{R_1} \times R_3$$

$$\begin{aligned} \text{(vi)} \quad R_4 &= \frac{50}{100} \times 82 \\ &= 41 \Omega \end{aligned}$$

(c) For R_1 1000 Ω resistor
For R_2 0 - 100 Ω resistance box
For R_3 10 Ω resistor (all - 02)

(any two - 01)

(d) zero OR No change

B - PART

01. (a) (i) nonviscous
Streamline / steady
Incompressible

03

(ii) Dimensions of $P = \frac{MLT^{-2}}{L^2}$

$$[PV^2] = ML^{-3} (LT^{-1})^2$$

$$= ML^{-1}T^{-2}$$

01

$$[Pgh] = ML^{-3}LT^{-2}L$$

$$= ML^{-1}T^{-2}$$

01

Equation is dimensionally Correct

(b) (i) P_1 and P_2 - Pressures at points A (B) & C
 V - the minimum speed with which the plunger should be pushed
 V_1 - the speed of air at point C

Bernoulli's equation : (A and C)

$$P_1 + \frac{1}{2} \rho V^2 = P_2 + \frac{1}{2} \rho V_1^2$$

02

(ρ - Density of air) [OR $P_1 + \frac{1}{2} \times 2V^2 = P_2 + \frac{1}{2} \times 2V_1^2$]

But $P_1 - P_2 = h\rho g$ (ρ - Density of liquid)

OR

$$P_1 - P_2 = 90 \times 10^{-3} \times 10^3 \times 10$$

02

From equation of Continuity

$$A_1 V_1 = A_2 V_2$$

$$60^2 V = 2^2 V_1 \text{ OR } \left(\frac{60}{2}\right)^2 V = (2/2)^2 V_1 \text{ OR } \pi \left(\frac{60}{2}\right)^2 V = \pi (2/2)^2 V_1$$

02

$$V_1 = 30^2 V$$

Form the first two equ

$$P_1 - P_2 = \frac{1}{2} \rho (V_1^2 - V^2)$$

$$900 = \frac{1}{2} \times 3 (30^4 V^2 - V^2)$$

01

$$30^4 V^2 \gg V^2$$

$$900 = 30^4 V^2$$

$$V^2 = \frac{900}{30^4}$$

$$V = \frac{1}{30} \text{ ms}^{-1} \text{ (or } 3.3 \text{ cms}^{-1})$$

01

(ii) Since the plunger is moving at a Constant Velocity the applied force is equal to the resistive force

The required force = 20 N

01

(02) (i) 20Hz - 20,000 Hz

(ii) Advantages

- ♦ Ultrasound is not known to produce any damage OR undesirable Side - effects to humans.
- ♦ Ultrasound does not ionize atoms OR molecules in human cells.
- ♦ Ultrasound is reflected by objects of small size

any two 01

- (iii) Ultrasound is a longitudinal wave 01
 (iv) Ultrasound are sound waves whose frequencies are above 20kHz OR above the audible range OR not audible to humans 01

- (v) ultrasound is not an electromagnetic wave 01
 Reason :
 It is a mechanical wave OR
 the speed of it is not equal to the speed of light in air OR
 needs a medium to travel 01

- (vi) (a) wavelength - λ
 $V = f\lambda$
 $\lambda = \frac{1500}{15 \times 10^6}$
 $\lambda = 10^{-4} \text{ m}$ 01

- (b) The value of the wave length is comparable to the size of the object concern. 01

- (vii)(a) $V \cos \theta$ 01

(b) $f' = f_1 \frac{(u + v \cos \theta)}{u}$ 01

(c) $f_r = f_1 \frac{u}{(u - v \cos \theta)}$ 01

$f_d = f_r - f_1 = f_1 \left(\frac{u + v \cos \theta}{(u - v \cos \theta)} - 1 \right)$ 01

$f_d = f_1 \left(\frac{u + v \cos \theta - u + v \cos \theta}{u - v \cos \theta} \right)$

$f_d = f_1 \frac{2 v \cos \theta}{(u - v \cos \theta)}$

- (viii) $8 \times 10^3 = \frac{2 \times 15 \times 10^6 V}{1500}$
 $V = 0.4 \text{ ms}^{-1}$ 01
 $(0.39 - 0.41 \text{ ms}^{-1})$

- (ix) To achieve a bigger value for f_d OR
 to achieve a practically measurable for f_d OR
 if θ is large f_d will be small 01

- (x) To mini-mize the reflection of ultrasound from the skin OR
 to maximize the transmission of ultrasound through the skin OR
 to provide a close coupling between the device and the skin OR
 to exclude air between the device and the skin 01

03. (i) Induced charge on the inner surface = $-1 \mu\text{C}$ }
 Induced charge on the outer surface = $+1 \mu\text{C}$ } 01

(ii) $E_r = \frac{Q}{4\pi\epsilon_0(OP)^2} = \frac{(1 \times 10^{-6}) \times (9 \times 10^9)}{0.2^2}$ 01
 $= 2.25 \times 10^5 \text{ NC}^{-1}$ 01

$E_s = \frac{Q (=0)}{4\pi\epsilon_0(OQ)^2}$
 $= 0$ - 01

$E_t = \frac{Q}{4\pi\epsilon_0(OT)^2} = \frac{(1 \times 10^{-6}) \times (9 \times 10^9)}{0.05^2}$
 $= 3.6 \times 10^6 \text{ NC}^{-1}$ 01



(iii) (a) $V_r = \frac{Q}{4\pi\epsilon_0(OP)} = \frac{(1 \times 10^{-6}) \times (9 \times 10^9)}{0.2}$
 $= 4.5 \times 10^4 \text{ V}$ - 01
 $V_Q = \frac{Q}{4\pi\epsilon_0(OQ)} = \frac{(1 \times 10^{-6}) \times (9 \times 10^9)}{0.15}$
 $= 6.0 \times 10^4 \text{ V}$ - 01

Since the electric field inside the conductor is zero

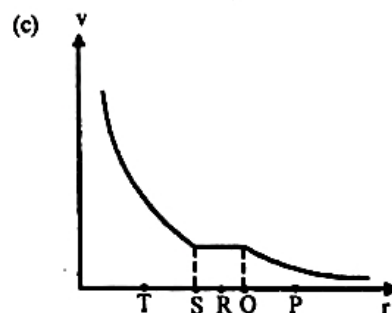
$V_R = V_Q = 6.0 \times 10^4 \text{ V}$
 $V_S = V_Q = 6.0 \times 10^4 \text{ V}$ } - 01

- (b) Potential difference between T and S

$\Delta V = V_T - V_S = \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{OT} - \frac{1}{OS} \right)$ 01
 $= (1 \times 10^{-6}) \times (9 \times 10^9) \left[\frac{1}{0.05} - \frac{1}{0.1} \right]$
 $= 9.0 \times 10^4 \text{ V}$ 01
 $\therefore V_T = (6.0 + 9.0) \times 10^4$
 $= 15.0 \times 10^4 \text{ V}$ 01

Alternative method

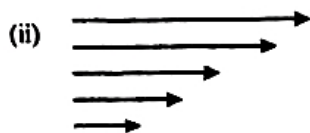
$V_T = \left[\frac{Q}{4\pi\epsilon_0 \times (0.05)} - \frac{Q}{4\pi\epsilon_0 \times (0.10)} + \frac{Q}{4\pi\epsilon_0 \times (0.15)} \right]$ - 01
 $V_T = (1 \times 10^{-6}) (9 \times 10^9) \left[0.05 + \frac{1}{0.15} - \frac{1}{0.1} \right]$
 $V_T = 15 \times 10^4 \text{ V}$ - 01
 $\Delta V = V_T - V_S = 15.0 \times 10^4 - 6.0 \times 10^4 \text{ V}$
 $= 9.0 \times 10^4 \text{ V}$ - 01



- (iv) Added charge does not reside on the inner surface
 $\therefore$ induced charge density of inner surface = $\frac{-1}{4\pi(OS)^2}$
 $= -7.96 \mu\text{cm}^{-2}$
 $= [-7.96 - 8.0 \mu\text{cm}^{-2}]$

Induced charge density of outer surface = 0 01

(04) (i) $F = \eta A \frac{V}{d}$ 01



02

(iii) (a) $F = \eta A \frac{V}{d}$ 01
 $0.05 = \eta \times 10^{-2} \times \frac{0.01}{10^{-3}}$ 01

$\eta = 0.5 \text{ Nsm}^{-2} (\text{kgm}^{-1}\text{s}^{-1})$

(Deduct 01 mark the unit is wrong)

(b) $F = \mu R$ 01

$R = mg$ OR $R = 0.5 \times 10$ 01

$\mu = \frac{0.05}{5}$ 01

$\mu = 0.01$ 01

(c) Rate of work done = Fv 01

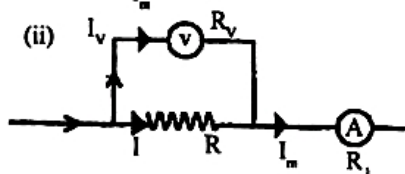
Energy that can be saved in one second

$= 0.25 \times 0.01 - 0.05 \times 0.01$ 01

$= 0.002 \text{ J}$ 01

(d) Additional downward force is acted on the block due to the Surface tension forces. (02 or zero)

05. (a) (i) $R = \frac{V_m}{I_m}$ 01



$I = I_m - I_v$ 01

$R = \frac{V_m}{I_m - I_v}$ 01

$R = \frac{V_m}{I_m - \frac{V_m}{R_v}}$ OR $R = \frac{V_m R_v}{I_m R_v - V_m}$ 01

Alternative Method

Let R_e be the equivalent resistance of R and R_v

$V_m = I_m R_e$ - 01

$R_e = \frac{R_v R}{R_v + R}$ - 01

$V_m = \frac{I_m R_e R}{R_v + R} \Rightarrow R = \frac{V_m R_v}{I_m R_v - V_m}$ - 01

(iii) At 30°C $V_m = 4.0 \text{ V}$ and $I_m = 0.02 \text{ A}$

$\therefore R = \frac{4.0 \times 1000}{0.02 \times 1000 - 4.0}$ 01

$= 250 \Omega$ 01

At 430°C $V_m = 4.05 \text{ V}$ and $I_m = 0.018 \text{ A}$

$\therefore R = \frac{4.05 \times 1000}{0.018 \times 1000 - 4.05}$

$= 290 \Omega$ (290.3 Ω) 01

Temperature Coefficient of resistivity α is given by

$R_\theta = R_0 (1 + \alpha (\theta - 0))$

$250 = R_0 (1 + \alpha (30 - 0))$ 01

$290 = R_0 (1 + \alpha (430 - 0))$ 01

$\frac{250}{290} = \frac{1 + 30\alpha}{1 + 430\alpha}$

$\alpha = 4.0 \times 10^{-4} \text{ } ^\circ\text{C}^{-1}$ 02
 $(4.0 - 4.1 \times 10^{-4} \text{ } ^\circ\text{C}^{-1})$

(iv) Applying Kirchhoff's law for the circuit

$E = V_m + I_m R_i$ 01

At 30°C $V_m = 4.0 \text{ V}$ and $I_m = 0.02 \text{ A}$

$E = 4.00 + 0.02 R_i$ 01

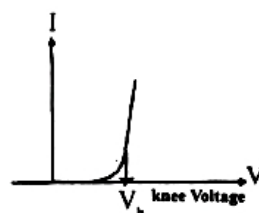
At 430°C $V_m = 4.05 \text{ V}$ and $I_m = 0.018 \text{ A}$

$E = 4.05 + 0.018 R_i$ 01

$R_i = 25 \Omega$ 01

$E = 4.5 \text{ V}$ 01

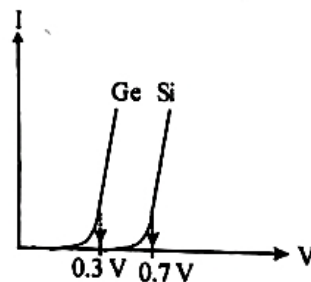
(b) (i)



01

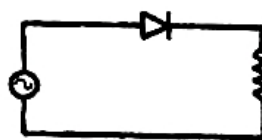
Knee voltage of Si is 0.7 V ($0.5 \text{ V} - 0.7 \text{ V}$)

Knee voltage of Ge is 0.3 V ($0.2 \text{ V} - 0.3 \text{ V}$)

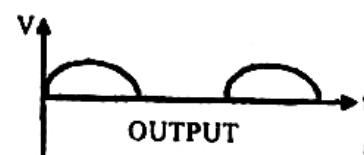
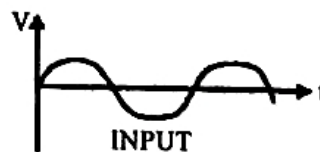


01

(ii)



01



both correct - 01

$$(iii) \text{ Peak current } I = \frac{25 - 0.7}{640} \left[\text{OR } I = \frac{25 - 0.6}{640} \right] \\ = 38 \text{ mA OR } 40.5 \text{ mA} \quad 01$$

$$\text{Peak output Voltage} = 600 I \text{ OR } 25 - 0.7 \\ = 22.8 \text{ V OR } 24.3 \text{ V} \quad 01$$

(iv) Current through the potential divider

$$I = \frac{12}{(10 + 2)} \times 10^{-3} \\ = 1.0 \text{ mA}$$

$$I_B = I/20 = \frac{1}{20} \text{ mA} \\ = (50 \pm 1) \mu\text{A} \quad 01$$

$$V_B = 1 \times 10^{-3} \times 2 \times 10^3 \\ = 2.0 \text{ V} \quad 01$$

$$V_E = 2.0 - 0.7 \text{ OR } 2.0 - 0.6 \\ = 1.3 \text{ V OR } 1.4 \text{ V} \quad 01$$

$$I_E = \frac{1.3}{1 \times 10^3} \text{ OR } \frac{1.4}{1 \times 10^3}$$

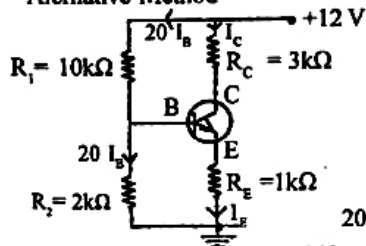
$$I_E = 1.3 \text{ mA} \quad (1.2 - 1.5 \text{ mA}) \quad 01$$

$$I_C \approx I_E = 1.3 \text{ mA} \quad 01$$

$$V_C = V_{CC} - I_C R_C \\ = 12 - 1.3 \times 10^{-3} \times 3 \times 10^3 \\ = 8.1 \text{ V (7.8 V)} \quad 01$$

$$V_{CE} = V_C - V_E = 8.1 - 1.3 \text{ OR } 7.8 - 1.4 \\ = 6.8 \text{ V (6.4 V)} [\pm 0.5 \text{ V}] \quad 01$$

Alternative Method



$$20I_B \times R_1 + 19I_B \times R_2 = 12 \quad 01 \\ \text{OR } 20I_B \times 10 \times 10^3 + 19I_B \times 2 \times 10^3 = 12$$

$$I_B = (50 \pm 1) \mu\text{A} \quad - 01$$

$$20I_B \times R_2 = 0.7 + I_E R_E \quad 02$$

$$20I_B \times 2 \times 10^3 = 0.7 + I_E \times 10^3$$

[01 mark for the L.H.S Other mark for the correct eq]

$$I_E = (1.2 \pm 0.2) \text{ mA} \quad 01$$

$$I_C \approx I_E = (1.2 \pm 0.2) \text{ mA} \quad 01$$

$$\text{OR } I_E = I_C + I_B$$

$$I_C R_C + V_{CE} + I_E R_E = 12 \quad \text{OR} \quad 02$$

$$(1.2 \pm 0.2) \times 10^{-3} \times 3 \times 10^3 + V_{CE} + (1.2 \pm 0.2) \times 10^{-3} \times 10^3 = 12$$

$$V_{CE} = (7.2 \pm 0.5) \text{ V} \quad 01$$

$$06. (a) (i) \text{ Steam Production Rate} = \frac{20 \times 10^3}{2.3 \times 10^4} \quad 01 \\ = 8.7 \times 10^{-3} \text{ kgs}^{-1} \quad 01 \\ (\text{or } 8.7 \text{ gs}^{-1}) \\ (8.7 \pm 0.1)$$

$$(ii) \text{ Applying } \frac{Q}{t} = kA \frac{(\theta_1 - \theta_2)}{d} \quad 01 \\ \text{Let } \theta \text{ be the temperature of the outer Surface}$$

$$20 \times 10^{-3} = \frac{400 \times 500 \times 10^{-4} (\theta - 100)}{2 \times 10^{-2}} \quad 03$$

$$\theta = 120^\circ\text{C} \quad - 01 \quad \text{One mark for R. H.S one mark for equating one mark taking Temperature of the boiling water as 100}$$

$$(iii) \text{ Steam Production is same as above} \quad 01 \\ \text{OR } 8.7 \times 10^{-3} \text{ kgs}^{-1}$$

$$(iv) \text{ Let } \theta^1 \text{ be the new temperature of the outer surface and } \theta_1 \text{ be the temperature of the interface}$$

$$20 \times 10^{-3} = \frac{400 \times 500 \times 10^{-4} (\theta^1 - \theta_1)}{2 \times 10^{-2}}$$

$$20 \times 10^{-3} = \frac{10 \times 500 \times 10^{-4} (\theta_1 - 100)}{10^{-3}} \quad 01$$

$$\theta_1 = 140^\circ\text{C}$$

$$\text{Then } 20 \times 10^{-3} = \frac{400 \times 500 \times 10^{-4} (\theta^1 - 140)}{2 \times 10^{-2}} \quad 01$$

$$\theta^1 = 160^\circ\text{C} \quad 02$$

(v) (1) No

Water will boil because all the generated heat will be absorbed by water at the steady state.

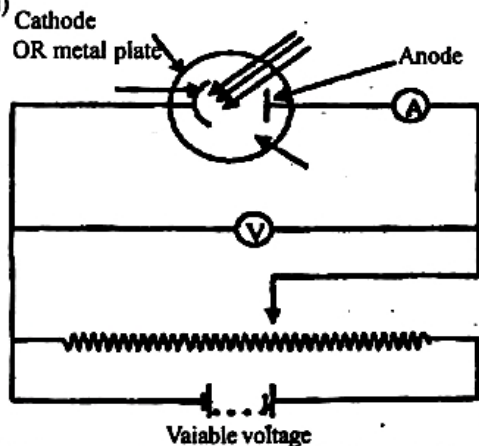
OR

There will be no loss of heat and therefore it is impossible to maintain the temperature at 50°C .

(2) yes

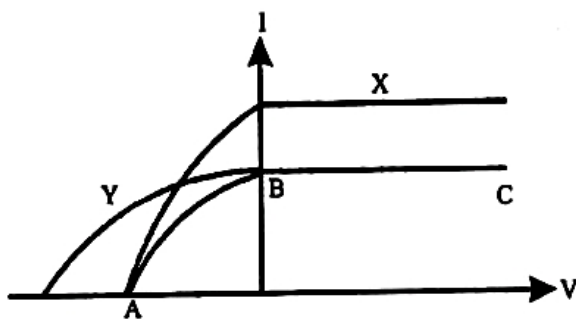
Part of the generated heat will be lost to the surroundings and steady state could be reached so that the temperature of water is 50°C .

(b) (i)



Circuit 01
labeling 01

(i)



AB part of the curve

01

BC part of the curve

01

Curve X

01

Curve Y

01

(ii) (1) $hf_0 = \phi$

01

$$c = f\lambda$$

01

OR
$$\left[\frac{hc}{\lambda_{\max}} = \phi \right]$$

02

$$\lambda_{\max} = \frac{6.63 \times 10^{-34} \times 3.0 \times 10^8}{4.08 \times 1.6 \times 10^{-19}}$$

01

$$\lambda_{\max} = 305 \text{ nm} \quad (3.05 \times 10^{-7} \text{ m})$$

$$(305 \pm 2) \text{ nm}$$

01

(2) Stopping potential V_s is given by

$$eV_s = \frac{1}{2} m V_{\max}^2 \quad (1/2 mv^2)$$

01

But $\frac{1}{2} m V^2 = \frac{hc}{\lambda} - \phi$

01

$$V_s = \frac{6.63 \times 10^{-34} \times 3 \times 10^8}{220 \times 10^{-9} \times 1.6 \times 10^{-19}} - 4.08$$

01

$$V_s = 1.6 \text{ V} \quad (1.6 \pm 0.1) \text{ V}$$

01

$$\frac{1}{2} m V_{\max}^2 = eV_s$$

$$V_{\max}^2 = \frac{2eV_s}{m}$$

$$V^2 = \frac{2 \times 1.6 \times 10^{-19} \times 1.6}{9.11 \times 10^{-31}}$$

$$V = 7.4 \times 10^5 \text{ ms}^{-1}$$

OR
$$V^2 = 2/m (hc/\lambda - \phi)$$

$$V^2 = \frac{2}{9.11 \times 10^{-31}} \left[\frac{6.63 \times 10^{-34} \times 3 \times 10^8}{220 \times 10^{-9}} - 4.08 \times 1.6 \times 10^{-19} \right]$$

$$= 7.4 \times 10^5 \text{ ms}^{-1}$$